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DATA REPORT FOR A TEST PROGRAM TO STUDY TRANSONIC FLOW FIELDS ABOUT AIRCRAFT WITH APPLICATION TO EXTERNAL STORES

VOLUME I. - SUMMARY REPORT, TUNNEL-EMPTY AND MACH-NUMBER SURVEY DATA, FORCE AND MOMENT DATA, AND PRESSURE DATA

> By Stanley C. Perkins, Jr., Stephen S. Stahara and Michael J. Hemsch

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TRANSONIC FLOW WIND TUNNEL MEASUREMENTS STORES WALL INTERFERENCE STORE CARRIAGE

FLOW FIELD MEASUREMENTS

EXTERNAL STORES

20. ABSTRACT (Construe on reverse side if necessary and identify by block number)

A test program was conducted to obtain measurements of flow velocities and static pressures in the vicinity of wing-body-store model (representative of a fighter-type aircraft) as well as surface pressures, forces, and moments on the model. Flow velocities and static pressures were also measured near the tunnel walls to provide outer flow field information. This report presents the data obtained during the test program conducted in the 4T and 16T Wind Tunnels at Arnold Engineering Development Center. The Flow-field data were obtained at Mac numbers 0.925, 0.975, and 1.025 and constitute the major part of the data. (conVolume I is a summary report which gives detailed information on the test program and presents uncertainties associated with the various types of data taken in the 4T Wind Tunnel. The volume also presents tunnel-empty and Mach-number surveys, as well as tabulated force and moment and pressure data for the Mach number range 0.80 to 1.15 and angles of attack -2°, -5°, 0°, 2°, and 5°. Volumes II, III, and IV present the tabulated flowfield data for the 4-percent thick wing model at Mach numbers 0.925, 0.975 and 1.025, respectively. Volume V presents the tabulated flow-field data for the 6-percent thick wing model, and Volume VI presents data obtained for the 4-percent thick wing model in the 16T Wind Tunnel.

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NOMENCLATURE

This section provides a list of symbols which identify various aerodynamic parameters, axis designations, subscripts, and tabulated data nomenclature.

indel sidewadh anda, dest tun" [[vr/vm]/[un/vm]]

Symbols

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AAL and ad	local upwash angle, deg; tan [(WL/VM)/(UL/VM)	1
AW SOS (4)	planform area of both wings (does not include body), 0.4444 ft2	¥
b	wing span, 16 in. notes meanin-soni	N
e niela	local wing chord	. y . y
a III de e	reference length for pitching moment, 5.3444 i	n.
CA filpiro i	X direction, axial force/ $q_{\infty}A_{W}$	ive
C. patw el	rolling-moment coefficient, positive left wind down as seen by pilot, rolling moment/q _∞ A _W b	, , , y ·
Cm; yalw a	pitching-moment coefficient, positive nose up seen by pilot, pitching moment/q _w A _W C	as
C _N we wood	normal-force coefficient, positive in the positive direction, normal force/ $q_{\infty}A_{\widetilde{W}}$	lt iv e
c _n store	yawing-moment coefficient, positive nose left seen by pilot, yawing moment/ $q_{\infty}A_{W}^{}$	as
Cp	local pressure coefficient, (p _l - p)/q _∞	. 0
cy paught	side-force coefficient, positive in the positive Y direction, side force/ $q_{\infty}A_{\widetilde{W}}$	lve 0
D	probe diameter, in.	
M	Mach number	
p	free-stream static pressure, psfa	
q	dynamic pressure, $\frac{1}{2} \rho V^2$, psf	***

identify r	radius of the body, in.
Re/ft	free-stream Reynolds number per foot, ft-1
SWL	local sidewash angle, deg; tan [(VL/VM)/(UL/VM)]
t	airfoil thickness, see figure 3
UL,VL,WL (1) \ (1)	local velocity components positive in the positive X, Y, and Z directions, respectively, ft/sec
v	total velocity, ft/sec
VM	free-stream velocity, ft/sec
x, y, z , m, apse, c	body-fixed Cartesian coordinates with origin coincident with the aircraft model nose at all angles of attack, see figure 6(a)
XT,YT,ZT	tunnel-fixed Cartesian coordinates with origin coincident with the aircraft model nose at zero angle of attack, see figure 6(b)
Y ₁ ,Z ₁ d ₁ , D ₂	coordinates of wing trailing edge at the wing root, in.; see figure 10
Y2,Z2	coordinates of wing trailing edge at the wing tip, in.; see figure 10
e a idleog édő a	angle of attack of model, angle between body axis and tunnel axis as defined in figure 7
^a probe of acon	angle of attack of probe, angle between probe axis and tunnel axis
Δ	increment along XT, YT, or ZT axis, see Table II
evities and	azimuthal angle in the Y-Z plane, deg; measured from the positive Y axis as shown in figure 6
	mass density, slugs/ft ³
	Subscripts
	Mach methor

l local conditions

Tunnel-Empty	Survey	Data	Tabulations	
--------------	--------	------	-------------	--

AATL	upwash angle referenced to tunnel-axis coordi-
bobslands	nates, calculated from probe measurements,
	deg; tan (WT/VT)
ALFA	aircraft-model angle of attack, positive nose up
	as seen by the pilot (nose down in tunnel), deg

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CPL .	local	pressure	coefficient	calculated	irom	probe
			(DT P) /0			

心如计算

5753

DATE	calendar ti	me at which	data were	recorded
x el	the tumeles	hi edora mi	bion of th	http://
M	lannet brites	frag-etras	m Mach min	har

atura, "P

ML v	local M	Mach number	calculated f	rom probe	measure-
	ments		8-14	e see his	

P	wind tunnel free-stream static pressure, psfa
PART	sequential indexing number for referencing data; a

PL	local	static	pressure	calculated	from	probe	measure-
-theans atcaed	ments	, psfa	adle rofe	s deserge 11	201		dan.

POINT	sequential indexing number for referencing data	
	obtained during one part; indexes each time a ne	W
ALTER STORMOGER	set of data inputs is obtained	6 di 1 2 h

PT	wind tunnel free-stream total pressure, ps	fa
PTL MOXI	local total pressure measured by probe, ps	fa
Q Set	wind tunnel free-stream dynamic pressure,	psf

REX10-6	wind tunnel	free-stream	unit Reynol	lds number,
	millions pe	er foot		

RUN	identifier	ior	specific	user	test type	
SURVEY	identifier	for	specific	user	grid-survey	combination

SWTL	sidewash angle referenced to tunnel-axis coordi-
48.00	nates, calculated from probe measurements,
	deg; tan (VT/UT)

TEST	alpha-numeric	notation	for referencing	a specific
			ific test unit	

TT	wind tunnel free-stream total temperature, OF
UT,VT,WT	velocity components in the tunnel-axis X, Y, and Z directions, respectively, calculated from probe measurements, ft/sec
	wind tunnel free-stream velocity, ft/sec
VML indured in	local velocity calculated from probe measurements, ft/sec
WING	wing designation used for a specific part number
XT	location of the probe in the tunnel-axis X direction
YT ~91006	location of the probe in the tunnel-axis 'Y direction
psia TS	location of the probe in the tunnel-axis Z direction
-eressam ed	Mach-Number Survey Data Tabulations
AAL SJAD D	acy, can (mb/ob)
ALFA	aircraft-model angle of attack, positive nose up as seen by the pilot (nose down in tunnel), deg
CPL ATE	local-pressure coefficient calculated from probe measurements, (PL - P)/Q
DATE TRO	calendar time at which data were recorded
M ,395	wind tunnel free-stream Mach number
ML.	local Mach number calculated from probe measurements
PART desca	a constant throughout each survey
P	wind tunnel free-stream static pressure, psfa
PL sillooga	local static pressure calculated from probe measurements, psfa

POINT	sequential indexing number for referencing data obtained during one part; indexes each time a new set of data inputs is obtained
incluse	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
PT	wind tunnel free-stream total pressure, psfa
PTL	local total pressure measured by probe, psfa
Q Mi the 2	wind tunnel free-stream dynamic pressure, psf
REX10-6	wind tunnel free-stream unit Reynolds number, millions per foot
RUN PARABETOR	identifier for specific user test type
SURVEY	identifier for specific user grid-survey combina-
bess affagt	car tion error confilerent correstor
SWL	local sidewash angle referenced to body-axis
ibroos (bod)	coordinates, calculated from probe measurements, deg; tan (VL/UL)
unna vhod b	
TEST	deg; tan (VL/UL) alpha-numeric notation for referencing a specific test program in a specific test unit
TEST TO THE	deg; tan (VL/UL) alpha-numeric notation for referencing a specific test program in a specific test unit
TEST TT UL,VL,WL	deg; tan (VL/UL) alpha-numeric notation for referencing a specific test program in a specific test unit wind tunnel free-stream total temperature, of velocity components in the body-axis X, Y, and Z directions, respectively, calculated from probe
TEST TT UL,VL,WL VM	deg; tan (VL/UL) alpha-numeric notation for referencing a specific test program in a specific test unit wind tunnel free-stream total temperature, of velocity components in the body-axis X, Y, and Z directions, respectively, calculated from probe measurements, ft/sec
TEST TT UL,VL,WL VM VML WING	<pre>alpha-numeric notation for referencing a specific test program in a specific test unit wind tunnel free-stream total temperature, velocity components in the body-axis X, Y, and Z directions, respectively, calculated from probe measurements, ft/sec wind tunnel free-stream velocity, ft/sec local velocity calculated from probe measurements, ft/sec wing designation used for a specific part number</pre>
TEST TT UL,VL,WL VM VML WING	<pre>deg; tan 1 (VL/UL) alpha-numeric notation for referencing a specific test program in a specific test unit wind tunnel free-stream total temperature, of velocity components in the body-axis X, Y, and Z directions, respectively, calculated from probe measurements, ft/sec wind tunnel free-stream velocity, ft/sec local velocity calculated from probe measurements, ft/sec</pre>
TEST TT UL,VL,WL VM VML	<pre>alpha-numeric notation for referencing a specific test program in a specific test unit wind tunnel free-stream total temperature, OF velocity components in the body-axis X, Y, and Z directions, respectively, calculated from probe measurements, ft/sec wind tunnel free-stream velocity, ft/sec local velocity calculated from probe measurements, ft/sec wing designation used for a specific part number</pre>

Force and Moment and Pressure Data Tabulations

ALFA aircraft-model angle of attack, positive nose up as seen by the pilot (nose down in tunnel), deg

neline.	THICH
Ab does eex	area of model base, .038/85 It
W sleet was	planform area of both wings (does not include body), 0.4444 ft
b stee ,ed	wing span, 16 in.
ā lag ,esma	reference length for pitching moment, 5.3444 in.
CA verdence a	axial-force coefficient measured by balance, in body coordinates, axial force/QAW
CAB sq	base axial-force coefficient in body coordinates, $(P - \overline{P}_b)A_b/QA_W$
CAF	axial-force coefficient corrected for base effects, in body coordinates, CA - CAB
CLL TROME THE REPORT	rolling-moment coefficient in unrolled body coordinates, rolling moment/ $QA_W^{}$
CLMF	pitching-moment coefficient in unrolled body coordinates, pitching moment/QAWC
CLN 10 vocation	yawing-moment coefficient in unrolled body coordinates, yawing moment/QAWb
CNF long road p	normal-force coefficient in unrolled body coordinates, normal force/QA $_{\overline{W}}$
CPS N (N = 1,25)	surface-pressure coefficient at orifice N, (PS - P)/Q
CY .	side-force coefficient, side force/QAW
redaug drag M olimanib X si	wind tunnel free-stream Mach number
P	wind tunnel free-stream static pressure, psfa
$\overline{\overline{P}}_{\mathbf{b}}$	average base pressure, psfa
PART	sequential indexing number for referencing data; a constant throughout each sweep
PS	aircraft-model local surface pressure, psfa
pr peb (198	wind tunnel free-stream total pressure, psfa

NOMENCLATURE (Concluded)

Q	wind tunnel free-stream dynamic pressure, psf
REX10-6	wind tunnel free-stream unit Reynolds number, millions per foot
RUN	identifier for specific user test type
SURVEY	identifier for specific user grid-survey combination
TEST	alpha-numeric notation for referencing a specific test program in a specific test unit
TT .	wind tunnel free-stream total temperature, OF
VM	wind tunnel free-stream velocity, ft/sec .
WING	wing designation used for a specific part number

DATA REPORT FOR A TEST PROGRAM TO STUDY TRANSONIC FLOW FIELDS ABOUT AIRCRAFT WITH APPLICATION TO EXTERNAL STORES

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VOLUME I. - SUMMARY REPORT, TUNNEL-EMPTY
AND MACH-NUMBER SURVEY DATA, FORCE AND
MOMENT DATA, AND PRESSURE DATA

Total-empty surveys at

1. INTRODUCTION

The test program described in this report, authorized under Air Force Contract No. F44620-75-C-0047, was conducted for the purpose of obtaining experimental measurements of flow velocities and static pressures in the vicinity of wing-body models in addition to body surface pressures and forces and moments on the models. Flow velocities and static pressures were also measured near the tunnel walls to provide outer flow field information. The test program was conducted in the 4T and 16T Wind Tunnels at Arnold Engineering Development Center at Mach numbers ranging from 0.80 to 1.15. The flow-field data were obtained at Mach numbers 0.925, 0.975, and 1.025 and constitute the major part of the data.

This report presents the data obtained during the test program. This volume, Volume I, is a summary report which gives detailed information on the test program and presents uncertainties associated with the various types of data taken in the 4T Wind Tunnel. This volume also presents tunnel-empty and Mach-number surveys, as well as tabulated force and moment and pressure data for the Mach number range 0.80 to 1.15 and angles of attack -2°, -5°, 0°, 2° and 5°. Volumes II, III, and IV present the tabulated flow-field data for the 4-percent thick wing model at Mach numbers 0.925, 0.975 and 1.025, respectively. Volume V presents the tabulated flow-field data for the 6-percent thick wing model, and Volume VI presents data obtained for the 4-percent thick wing model in the 16T Wind Tunnel.

A summary of the test data contained in each volume is presented below.

<u>Volume</u>	Wind Tunnel	Wing	Test Data			
		ATAR LAN	MOMPH'S DATA, ATAG THEMOM			
I	4T	None	Tunnel-empty surveys at M ₂ = .80, .85, .90, .95, 1.0, 1.025, 1.05, 1.10, 1.15			
49.0	ted for te	4-percent	Mach-number surveys at $M = .80$, .85, .90, .95, 1.0, 1.025, 1.05, 1.10, 1.15 and $\alpha = 0^{\circ}$			
			to versionly and of essence of the vicinity of			
boat.		4-percent and 6-percent	Force and Moment and Pressure data at M = 0.80, 0.85, 0.90, 0.925, 0.95, 0.975, 1.0, 1.025, 1.05, 1.10, 1.15			
11 5 8	den 41 be	4-percent	Flow-field survey data at $M_{\infty} = 0.925$ and $\alpha = 0^{\circ}$, $\frac{+}{2}$, $\frac{+}{5}$			
	leum de bo d e deg is fant	840. (500) 42. (500) 100 (600) 51. (400) 100 (400) 100 (500) 100 (600) 100 (600) 100 (600) 100 (600)	Flow-field survey data at $M_{\infty} = 0.975$. and $\alpha = 0^{\circ}$, $\frac{1}{2}$, $\frac{1}{2}$, $\frac{1}{2}$			
	les detai	4-percent	Flow-field survey data at $M_{\infty} = 1.025$ and $\alpha = 0^{\circ}$, $\frac{+}{2}$, $\frac{+}{5}$			
	ainties as		and purposed read and an accommodati			
		6-percent	Flow-field survey data at $M_{\infty} = 0.925$, .975, 1.025, and $\alpha = 0^{\circ}$, $\pm 2^{\circ}$, $\pm 5^{\circ}$			
VI O	16T	None	Tunnel-empty surveys at M _∞ = .925, .975, 1.025			
	riedaula do uni grass Leira sei	4-percent	Force and Moment and Pressure data at $M_{\odot} = .80$, .85, .90, .925, .95 .975, 1.0, 1.025, 1.05, 1.10, 1.15 and $\alpha = 0^{\circ}$, $\frac{1}{2}$, $\frac{1}{2}$			
Tata linu	Holast samp	ateday right	or remeded the statement of Westley Day			
	ai soulo	4-percent	Flow-field survey data at $M_{\infty} = 0.925$, 0.975, 1.025 and $\alpha = 0^{\circ}$, $+ 5^{\circ}$			

presented below.

References 1 and 2 are reports prepared by AEDC describing data reduction procedures used in the 4T and 16T Wind Tunnel facilities, respectively, to determine force and moment, pressure, and flow-field data. The data uncertainties given in this report were provided by AEDC and meet the data quality requirements that were outlined in reference 3.

sure offices, & on the next norther and is on the fuselane

2. PURPOSE AND SCOPE OF TEST PROGRAM

The purpose of the test program is to obtain experimental. data which will aid in the development and evaluation of a theoretical method for predicting flow fields about three-dimensional configurations characteristic of modern fighter/bombers flying in the transonic range. The scope of the test program is to obtain data on a simplified wing-body combination with two different sets of wings at subcritical, supercritical, and supersonic speeds for several values of angle of attack. The effects of wall interference in the 4T Tunnel will also be studied by repeating several of the test conditions in the 16T Propulsion Wind Tunnel. Detailed information regarding these wind tunnels can be found in reference 4. The bulk of the testing was done in the 4T Tunnel and the data obtained from these tests comprise the major part of this data report. This volume, Volume I, summarizes the data, presents the 4T Tunnel-empty and Mach-number surveys, and presents some uncertainties associated with the data. Also, the force and moment and pressure data obtained in the 4T Tunnel are presented in this volume. The 4T Tunnel flow-field survey data are presented in Volumes II through V and all data obtained in the 16T Tunnel are presented in Volume VI.

3. TEST HARDWARE

The test installation consisted of a wing-body combination in whose proximity a flow-field survey probe was located. Flow-field survey, pressure distribution, and force and moment data were obtained for two wing-body combinations during the test program.

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The flow-field survey data was obtained using the AEDC 0.25-inch diameter conical probe with a 20° semi-apex angle. The body is an aluminum fuselage which was bored out and mounted on the 1.5-inch, 500 lb. AEDC 6-1.50-1.12 M-A balance. The force and moment data on the wing-body combinations were obtained using this balance. The entire body contained 25 axially-aligned pressure orifices, 6 on the nose portion and 19 on the fuselage section, from which pressure data on the body surface were obtained.

Figure 1 shows the wing-body combination with the 4-percent wing in the 4T Tunnel with the conical flow-field probe supported on the captive trajectory system (CTS, see ref. 4). Figure 2 is a drawing of the wing-body model which includes the positions of the 25 pressure orifices along the body centerline. Sketches and coordinates of the 4-percent and 6-percent thick airfoils which were used to obtain data are given in figure 3. A detailed sketch of the entire conical flow-field probe and of the probe tip are shown in figure 4. It is also noted that 0.0035-inch, \$150 Carbolum grit was used on the nose tip and wing leading edges to trip the boundary layer. Figure 5 shows the positions and width of the grit for both the body nose and wings.

4. DEFINITION OF AXES

A conventional set of orthogonal body-fixed axes is used as a frame of reference for the inner flow-field surveys near the body. The origin of the wing-body combination system is at the tip of the nose, as shown in figure 6(a). The pressure orifices are on the same side that probe measurements are taken, which is on the negative Z axis side. As seen by a person positioned on the pressure orifices and looking toward the nose, the X axis is positive aft, the Y axis is positive to the left and the Z axis is positive down.

obtained from the be teath compared the matter particol th

A conventional set of orthogonal tunnel-fixed axes is used as a frame of reference for the outer flow-field surveys near the

tunnel walls and is shown in figure 6(b). The origin of this reference frame is the nose of the model body when the wing-body is at an angle of attack of 0° . It is at this position that the body-fixed axes and tunnel-fixed axes coincide.

The sign convention adopted for the upwash and sidewash angles is shown in figure 7. In the figure, the wing-body is shown in the tunnel at a negative angle of attack to show the flow components with respect to the walls of the tunnel. In the body-axis system, positive angular values of sidewash and upwash correspond to positive values of their respective velocity components. As seen by a person positioned on the pressure orifices and looking forward, positive upwash is a downward flow and positive sidewash is an outward flow along the left wing panel.

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5. DESCRIPTION OF TESTS

Tests for which experimental data are reported herein are of three general types: (1) flow-field survey tests, (2) pressure-distribution tests and (3) force and moment tests. The tests have been conducted at nominal free-stream Mach numbers of 0.80 to 1.15 and at a nominal Reynolds number per foot of 3.0×10^6 . Tests were conducted with a 4-percent thick and a 6-percent thick airfoil to investigate thickness effects on the flow field generated by the wing-body combination.

A note is made here with respect to the positioning of the probe. The X and XT coordinates given in the tabulated data are the axial positions of the probe static pressure orifices in the body-axis and tunnel-axis systems, respectively. The Y and Z coordinates indicate the lateral and vertical positions of the probe longitudinal axis in the body-axis coordinate systems, while YT and ZT indicate the lateral and vertical positions of the probe longitudinal axis in the tunnel-axis coordinate system.

dies the the despread thick wind-mody combination as the same

5.1 Flow-Field Survey Tests The record of branch to the street formers

Flow-field survey tests were conducted with the tunnel empty and with two wing-body configurations at several angles of attack. The conical probe used in the tests was calibrated at nominal Mach numbers of 0.80, 0.85, 0.90, 1.0, 1:025, 1.05, 1.10, and 1.15. Tunnel-empty surveys were made at the same Mach numbers to investigate the uniformity of the free-stream conditions in the region of the wing-body model. Mach-number surveys were also taken in regions of particular interest with the wing-body model in the tunnel. The aforementioned conical probe was used to obtain flow-field velocity components and upwash and sidewash angles, as well as other quantities, at various locations of interest. The velocities and angles were calculated using five pressures measured with the probe. One is a total pressure, located on the tip of the probe, and the other four consist of two orthogonal pairs of static pressures located on the surface of the conical probe. These pressures have also been used to deduce other local-flow quantities, such as Mach number and total pressure. Flow-field surveys were obtained at Mach numbers 0.925, 0.975, and 1.025 for both the 4-percent thick and 6-percent thick wing-body combinations. Data were taken at specified spanwise and chordwise positions for angles of attack of 0°, + 2°, and + 5°.

The specific flow-field survey tests which were performed and the final data which were obtained are presented in Volumes I through VI of this report. Volumes I through V contain the data obtained in the 4T Tunnel and Volume VI contains data obtained in the 16T Tunnel. Volume I contains Tunnel-empty and Mach-number survey data at Mach numbers 0.80, 0.85, 0.90, 0.95, 1.0, 1.025, 1.05, 1.10 and 1.15. Volumes II, III, and IV contain data for the 4-percent thick wing-body combination at Mach numbers 0.925, 0.975, and 1.025, respectively, and Volume V contains data at the same Mach numbers for the 6-percent thick wing-body combination. Volume VI contains data for the 4-percent thick wing-body combination at the same

5.2 Pressure Distribution Tests and a region and a paper

Axial pressure distributions were obtained along the body surface for Mach numbers 0.80, 0.85, 0.90, 0.925, 0.95, 0.975, 1.0, 1.025, 1.05, 1.10 and 1.15 with the 4-percent thick wingbody combination and for Mach numbers 0.925, 0.975, and 1.025 with the 6-percent thick wing-body combination. The pressure distributions were obtained along the bottom of the body ($\alpha = 0^{\circ}$, 2° , and 5°) and along the top of the body ($\alpha = -2^{\circ}$ and -5°).

The specific pressure distribution tests which were performed and the final data which were obtained are presented in this volume, Volume I, for the 4T Tunnel and in Volume VI for the 16T Tunnel.

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by AMC and are presented below.

5.3 Force and Moment Tests Tests Till Wilder La August Angland and

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Force and moment data were obtained for the 4-percent thick wing-body combination at Mach numbers 0.80, 0.85, 0.90, 0.925, 0.95, 0.975, 1.0, 1.025, 1.05, 1.10 and 1.15 and for the 6-percent thick wing-body combination at Mach numbers 0.925, 0.975, and 1.025. These data were obtained for $\alpha = 0^{\circ}$, $\pm 2^{\circ}$, and $\pm 5^{\circ}$.

The specific force and moment tests which were performed and the final data which were obtained are presented in this volume, Volume I, for the 4T Tunnel and in Volume VI for the 16T Tunnel.

6. SYMMETRY OF TESTS

This section of the data report contains an assessment of the symmetry of the flow-field survey tests previously described in this report. Specifically, this refers to comparisons of data taken at points whose Z values are identical, but whose Y locations differ in sign only. These comparisons are a good measure of the exactness of positioning the wing-body configuration and probe with respect to one another, the symmetry of the configuration and flow field, and a check of the data reduction procedure.

Figure 8 shows comparisons of pressure (CD), upwash (AAL), and sidewash (SWL) for positions (4, -1), (-4, -1) and (7, -1), (-7, -1) at $\alpha = 0^{\circ}$ and M = 0.925 (4-percent thick wing). Figure 9 shows the same comparisons at M = 1.025. These comparisons were carried out for all Mach numbers and angles of attack and for both wings. With the exception of the upwash comparisons at the outboard positions, all comparisons for pressure, upwash and sidewash were very good. Several explanations for the poor upwash comparisons at the outboard positions are offered. First, the regions in which the comparisons are poor are regions in which the measured angle is very small, and the difference in the measurements is usually within the accuracy of the data (+ 0.40°, see DATA UNCERTAINTIES section). Second, the wings on either side of the fuselage have slightly different maximum thickness at the tips. Also, the difference between the vertical coordinates of the wing trailing edge at the tip and root is not the same on both sides. These differences, which are given in figure 10, could effect upwash measurements, although it is felt that it would be a very small effect. It is also possible that the flow field of the tunnel is not symmetric in the region of interest, as is shown in reference 5. A small difference in tunnel-empty upwash in the region of interest could easily cause the differences seen in upwash at the outboard wing position.

The overall good agreement shown in the comparisons indicates accurate positioning of the wing-body configuration in the tunnel and of the probe with respect to the wing-body model, and lends confidence to both the test procedures and data reduction schemes used to obtain this data.

7. DATA UNCERTAINTIES

Uncertainties in the aerodynamic coefficients, local conditions, flow angles, and probe position for the 4T Wind Tunnel were provided by ARO and are presented below.

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tadulated data for each tunnel-entity corpy, Column four indicates

Examining the uncertainties associated with probe angle (a probe) and upwash angle (AAL), there exists a maximum possible uncertainty of + 0.40°. This is the uncertainty mentioned in Section 6 that could account for the disagreement of upwash angle at the outboard position. The particular as the college alpha learned

8. TUNNEL-EMPTY SURVEYS THE BOOK THE BOOK TO

Figure 11 shows the grids used in the tunnel-empty surveys, which were taken at Mach numbers 0.80, 0.85, 0.90, 0.95, 1.0, 1.025, 1.05 and 1.10 and at a nominal free-stream Reynolds number per foot of 3.0×10^6 to ascertain the quality of the tunnel-empty flow field.

An example of the type of results derived from the tunnelempty surveys is the XT traverse at YT = 0.0, ZT = -14.14. The sidewash at this particular location should always be zero, since it lies in the plane of symmetry of the configuration. Examining the sidewash at $M_{m} = 0.90$ and 0.95, as shown in figure 12, it is seen to be nonzero. It could be argued at first that the "nonzero" sidewash is due to probe error, but closer inspection shows a consistent nonzero sidewash throughout the Mach number range. With the model in the tunnel, the same nonzero sidewash distribution is present throughout the Mach number and angle of attack range, as shown in figure 12. The consistency of these results offers reasonable proof that the tunnel-empty flow field has a slightly positive sidewash angle along (YT,ZT) = (0.0, -14.14). The nonzero sidewash is relatively small, however, and will therefore have very little effect on the data taken in this region. this same manner, the tunnel-empty upwash and sidewash in other parts of the flow field can be examined to determine their effects on the data taken in those regions.

The tunnel-empty surveys at $M_{\infty} = 0.80$, 0.85, 0.90, 0.95, 1.0, 1.025, 1.05 and 1.10 are summarized in Table II. Columns one and two indicate the page number and part number, respectively, of the tabulated data for each tunnel-empty survey. Column four indicates the free-stream Mach number. Columns five, six and seven indicate the XT, YT, and ZT ranges, respectively, for each traverse. Column nine indicates the increment for the axis along which the traverse is being carried out. All positions are relative to the tunnel origin, which is located at the tip of the wing-body model

when the model is at $\alpha = 0^{\circ}$.

The data are presented in tabular form on pages 1 through 36 at the end of this volume. The heading on each page contains the test number, the part number, the Reynolds number per foot, the angle of attack of the model (not applicable for these tests), the type of wing attached to the model (none for these tests), and the (YT,ZT), (XT,YT), or (XT,ZT) coordinates at which the probe traverse is carried out. Also included are the run and survey numbers and the date on which the data were recorded.

Below the heading information are the data obtained during The first two columns indicate the sequential indexing number for referencing data obtained during one part (POINT) and the location of the probe in the tunnel axis XT, YT, or ZT direc-The wind tunnel free-stream quantities are in columns three through seven, and are Mach number (M), velocity (VM, ft/sec), total pressure (PT, psfa), dynamic pressure (Q, psf), and total temperature (TT, OF). Following these quantities are local quantities as measured by the probe or calculated from probe measurements. These local quantities are Mach number (ML), the ratio of local to freestream velocity (VML/VM), the ratio of local to free-stream total pressure (PTL/PT), pressure coefficient (CPL), the ratio of local velocity components in the tunnel axis X, Y, and Z directions, respectively, to the free-stream velocity (UT/VM, VT/VM and WT/VM, respectively), and the upwash and sidewash angles referenced to tunnel-axis coordinates (AATL and SWTL, respectively). The positive sense of the upwash and sidewash is shown in figure 7.

9. MACH-NUMBER SURVEYS

The Mach-number surveys were taken at Mach numbers 0.80, 0.85, 0.90, 0.95, 1.0, 1.025, 1.05, 1.10 and 1.15 at a nominal Reynolds number per foot of 3.0×10^6 . These tests were taken with the 4-percent thick wing-body configuration at $\alpha=0^0$ along an X traverse at Y = 3.0, Z = -2.0 and -1.0. The purpose of these

tests was to establish appropriate subcritical and supercritical test conditions for the flow-field surveys.

The data are presented in tabular form on pages 37 through 56 of this volume. The heading on each page contains the test number, the part number, the Reynolds number per foot, the angle of attack of the model, the type of wing attached to the model (4-percent thick wing for the Mach-number surveys), and the Y and Z coordinates at which the X traverse is carried out. Also included are the run and survey numbers and the date on which data were recorded.

Below the heading information are the data obtained during The first two columns indicate the sequential indexing number for referencing data obtained during one part (POINT) and the location of the probe in the body-axis X direction. wind tunnel free-stream quantities are in columns three through seven and are Mach number (M), velocity (VM, ft/sec), total pressure (PT, psfa), dynamic pressure (Q, psf), and total temperature (TT, F). Columns eight through sixteen contain local quantities which were either measured by the probe or calculated from probe measurements. These local quantities are Mach number (ML), the ratio of local to free-stream velocity (VML/VM), the ratio of local to free-stream total pressure (PTL/PT), the pressure coefficient (CPL), the ratio of the local velocity components in the body-axis X, Y, and Z directions, respectively, to the freestream velocity (UL/VM, VL/VM, and WL/VM, respectively), and the upwash and sidewash angles referenced to body-axis coordinates (AAL and SWL, respectively). The positive sense of the upwash and sidewash is shown in figure 7.

10. FORCE AND MOMENT AND PRESSURE TESTS

This section presents the force and moment and pressure data at $M_{\infty} = 0.80$, 0.85, 0.90, 0.925, 0.95, 0.975, 1.0, 1.025, 1.05, 1.10 and 1.15 for the 4-percent thick wing-body and at $M_{\infty} = 0.925$,

0.975 and 1.025 for the 6-percent thick wing-body. Data for both wings is presented at $\alpha = 0^{\circ}$, $\pm 2^{\circ}$, $\pm 5^{\circ}$. These tests, performed at a nominal Reynolds number per foot of $3.0\times10^{\circ}$, are outlined in Table IV of this volume. The tabulated data are at the end of this volume beginning on the page numbered 57.

10.1 Description of Tests

The aerodynamic coefficients on the wing-body models were obtained during the force and moment tests using the 1.5-inch, 500 lb. AEDC balance $\sharp 6\text{-}1.50\text{-}0.50\text{-}1.12$ M-A. The fuselage was bored out and mounted on this balance. The surface-pressure data were obtained from the 25 pressure orifices on the body surface. The orifices are labeled 1 through 25 with number 1 being closest to the nose tip. The data are arranged such that there are two pages for each Mach number. The first presents the force and moment data for the angle-of-attack range $(0^{\circ}, \pm 2^{\circ}, \pm 5^{\circ})$ and the second presents the pressure data obtained at each angle of attack.

The force and moment and pressure tests are summarized in Table IV. Columns one and two indicate the page and part numbers, respectively, of the tabulated data. Column four indicates the Mach number. Column six indicates the type of data given on each page; F & M indicates force and moment data and P indicates pressure data. Column eight indicates which wing (4-percent thick or 6-percent thick) was attached to the body for each particular run.

10.2 Description of Data

The data are presented in tabular form on pages 57 through 84 of this volume. As previously mentioned, each Mach number has two pages of data associated with it. The first page contains force and moment data and the second contains pressure data. The heading on both pages is identical and contains the test number, the part

number, the free-stream Mach number, total pressure, static pressure, Reynolds number per foot, velocity, dynamic pressure, and total temperature. Also included are the type of wing attached to the body (4-percent thick or 6-percent thick), the run number and the survey number.

Below the heading on the first page of each Mach number section are the data obtained during each force and moment test. The results for the force and moment tests include the wing-body model angle of attack, the normal-force coefficient (CNF), the side-force coefficient (CY), the axial-force coefficient corrected for base effects (CAF), the pitching-moment coefficient (CLMF), the yawing-moment coefficient (CLN), the rolling-moment coefficient (CLL), and the base axial-force coefficient (CAB). The positive sense of these forces and moments is shown in figure 13.

Below the heading on the second page of each Mach number section are the data obtained during each pressure test. Column one indicates the orifice at which the pressure coefficient was measured. Columns two through six indicate the pressure coefficient at $\alpha = -5^{\circ}$, -2° , 0° , 2° and 5° , respectively, at each orifice location. The locations of the pressure orifices are shown in figure 2.

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TABLE I. - SUMMARY OF TABULATED DATA IN VOLUME I

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TABLE IV. - FORCE AND MOMENT AND PRESSURE TESTS

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Figure 1.- Conical flow-field survey probe on CTS and wing-body combination with 4-percent thick airfoil.

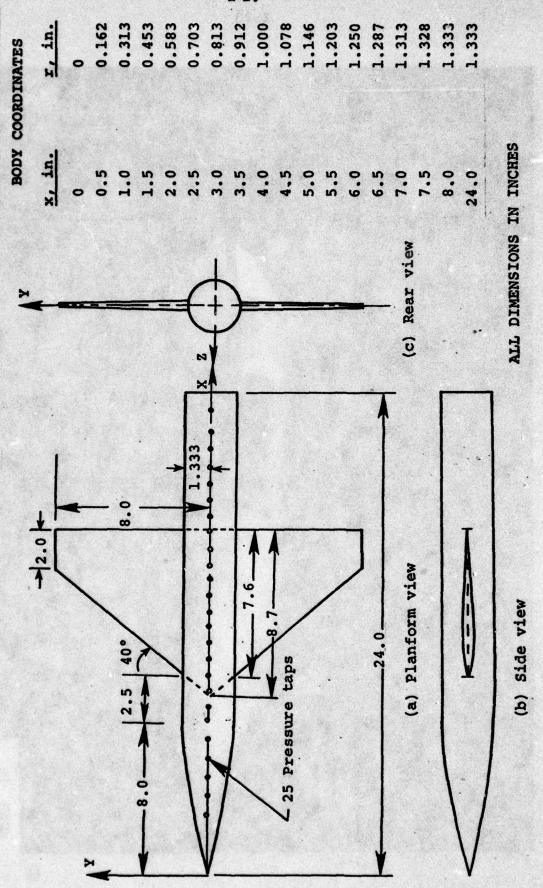


Figure 2.-Wing-body combination.

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(a) 4-percent thick airfoil

Figure 3.-Coordinates of airfoil sections.

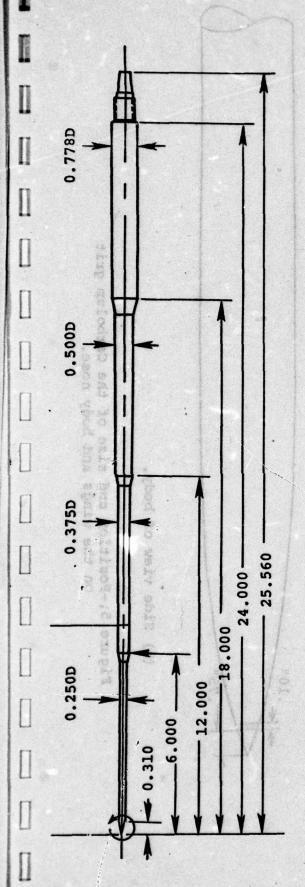
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5.0	1.313	2.5	
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(b) 6-percent thick airfoil (NACA 65A006)

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Figure 3.-Concluded.

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(a) Overall view of the probe.

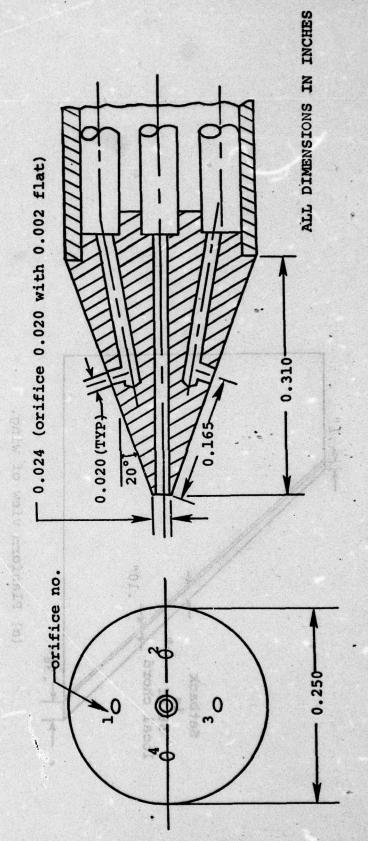
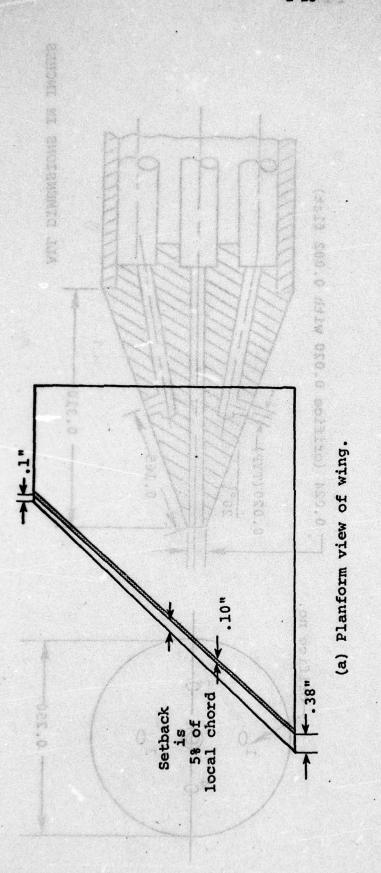
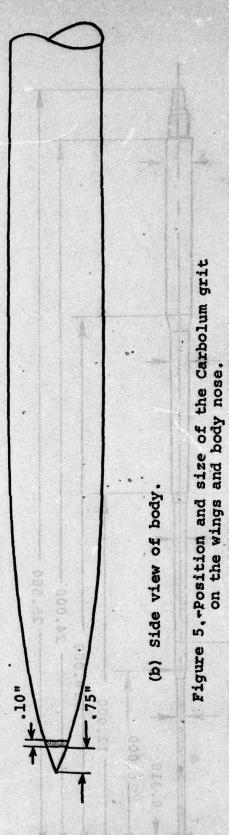
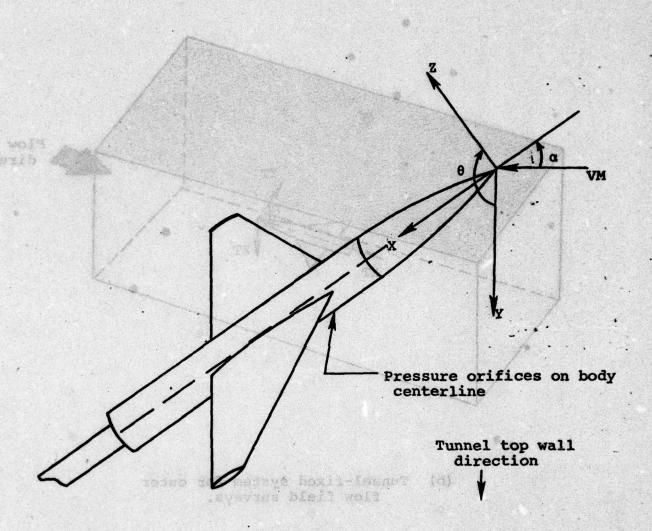


Figure 4.-Details and Dimensions of the 40° apex angle probe. (b) Details of the 40° probe tip.



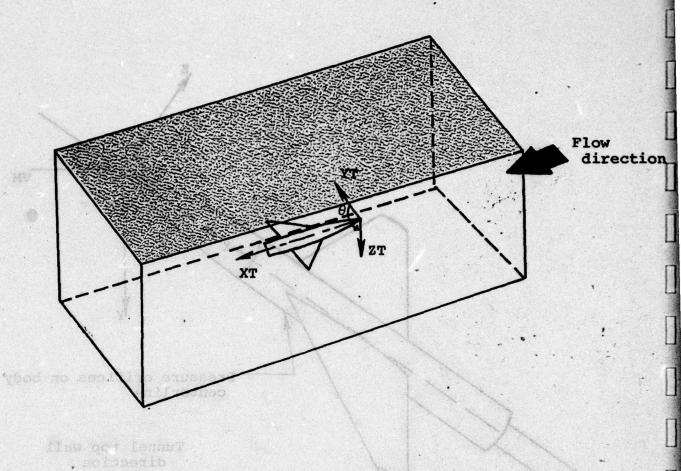
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(a) Body-fixed system for inner flow field surveys.

Figure 6.-Coordinate systems.



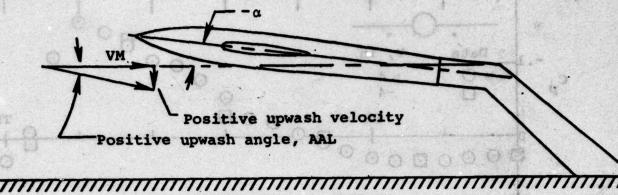
(b) Tunnel-fixed system for outer flow field surveys.

Figure 6.- Concluded.

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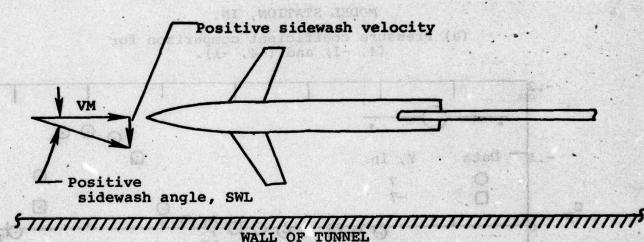
TOP WALL OF TUNNEL

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BOTTOM WALL OF TUNNEL

(a) Side view of tunnel.



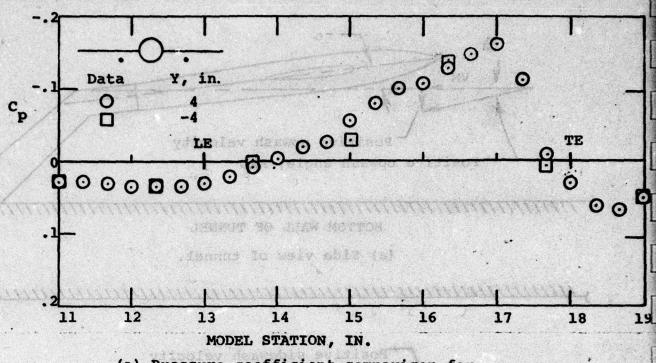
(b) Plan view of tunnel from top.

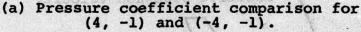
Figure 7.-Pictorial sign convention for upwash and sidewash angles.

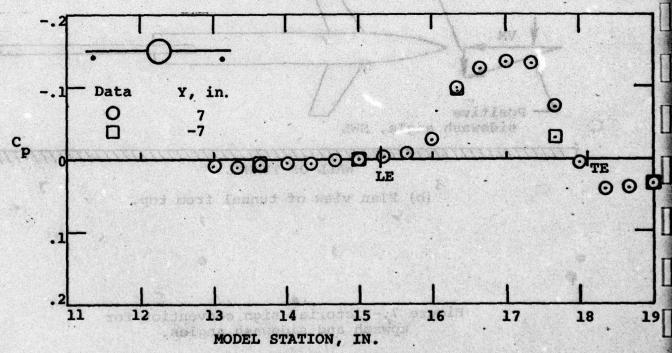
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TOP LEADS OF TUNNEL







(b) Pressure coefficient comparison for (7, -1) and (-7, -1).

Figure 8.-Symmetry comparisons for 4-percent thick wing-body combination at z=-1.0 in., $\alpha=0^{\circ}$, $M_{\infty}=0.925$.

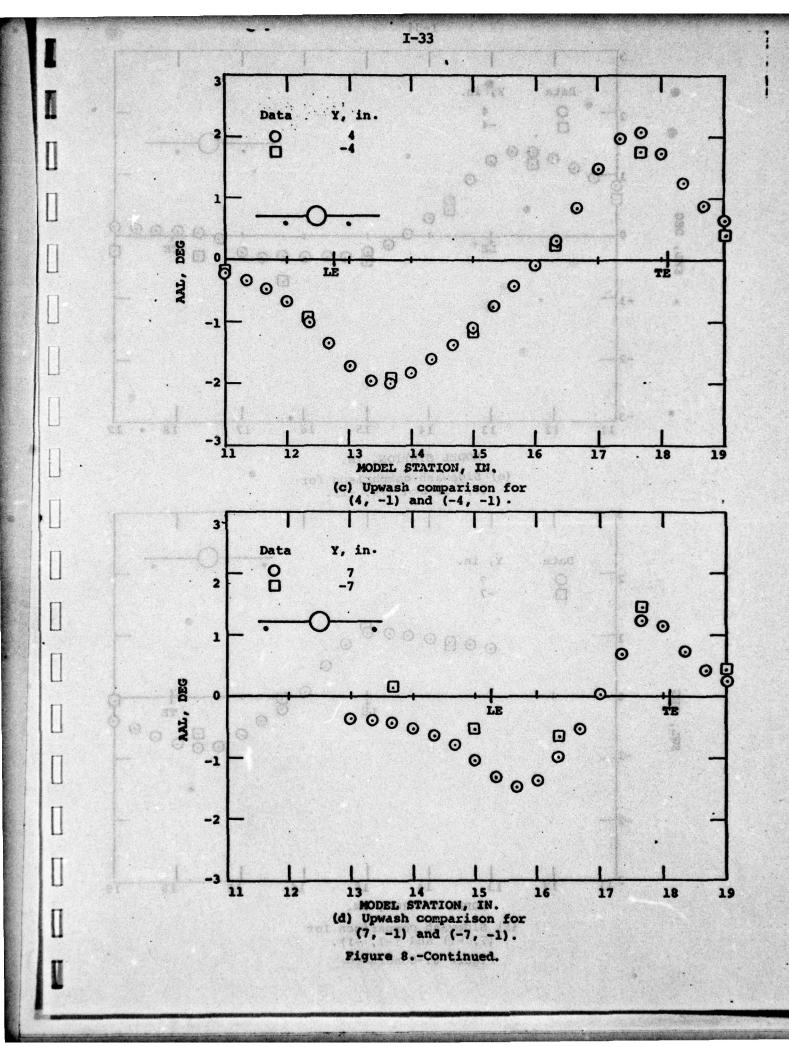


Figure 8.-Concluded.

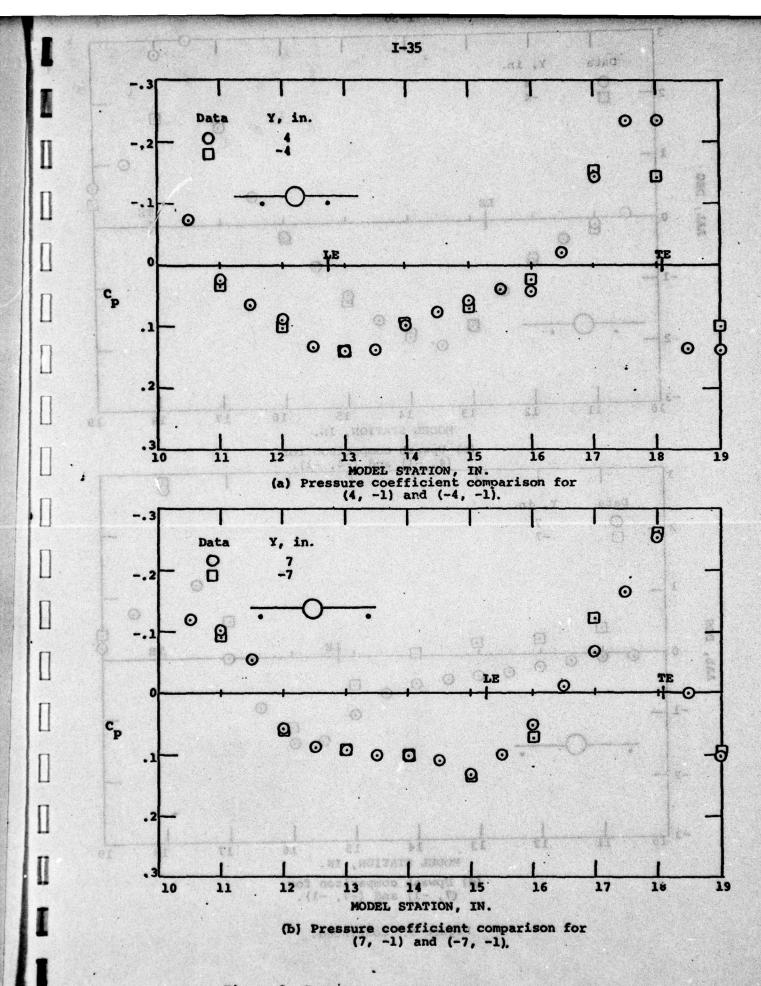


Figure 9.-Symmetry comparisons for 4-percent thick wing-body combination at Z=-1.0 in., $\alpha=0^{\circ}$, $M_{\odot}=1.025$.

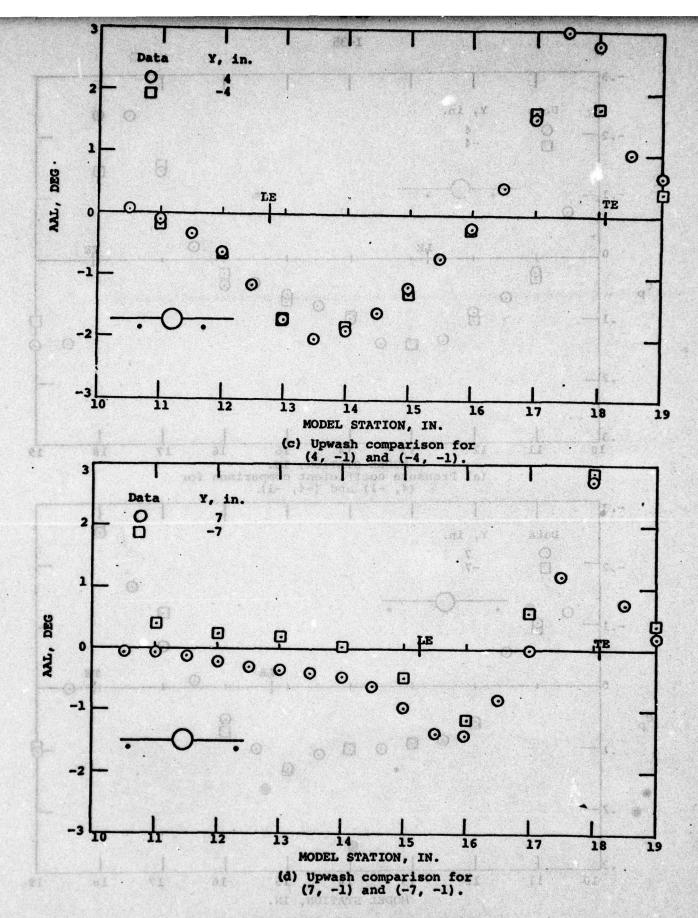
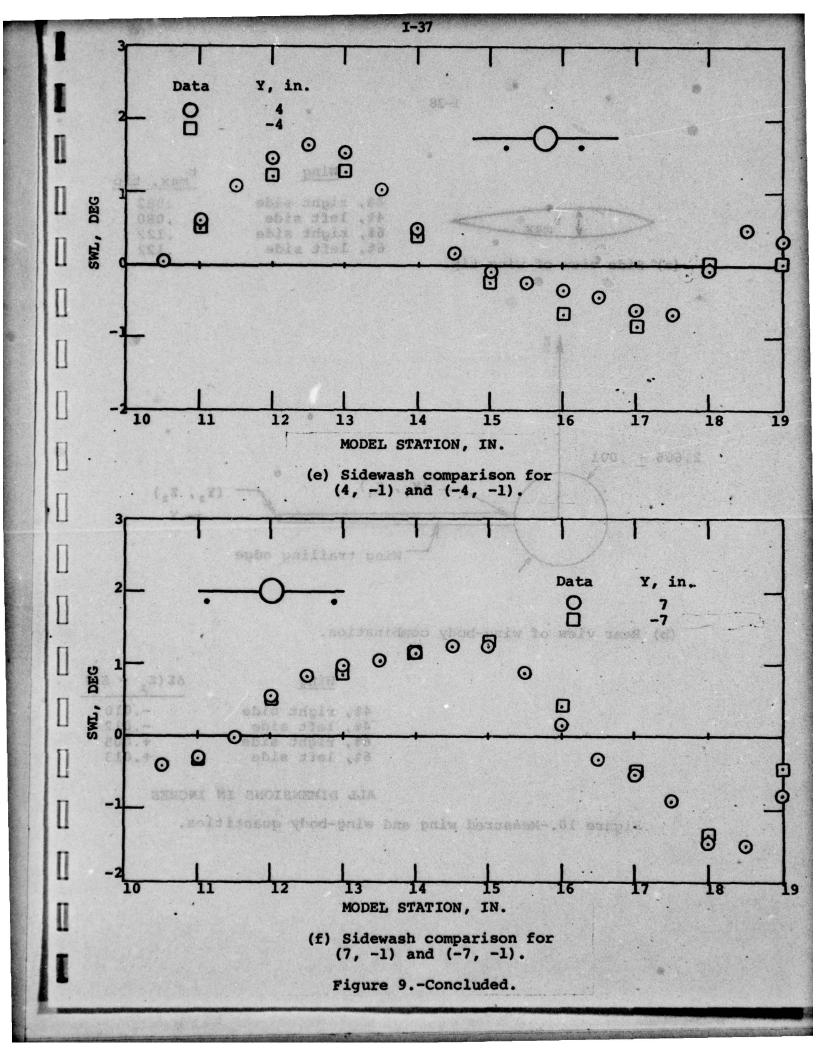


Figure 9.- Continued.

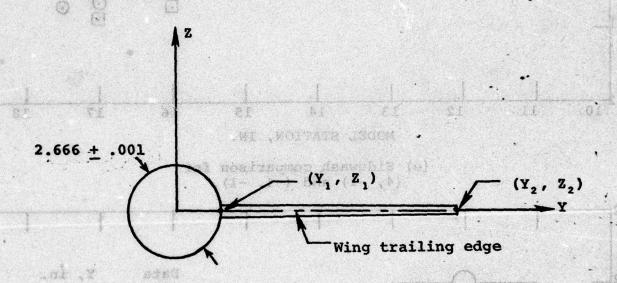
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(a) Side view of wing tip.

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	eft side	0.080
6%, r	ight side	.122
6%, 1	eft side	.122



(b) Rear view of wing-body combination.

Wing .	ΔZ (Z ₂ - Z ₁)
4%, right side	010
4%, left side	012
6%, right side	+.005
6%, left side	0 0+.013

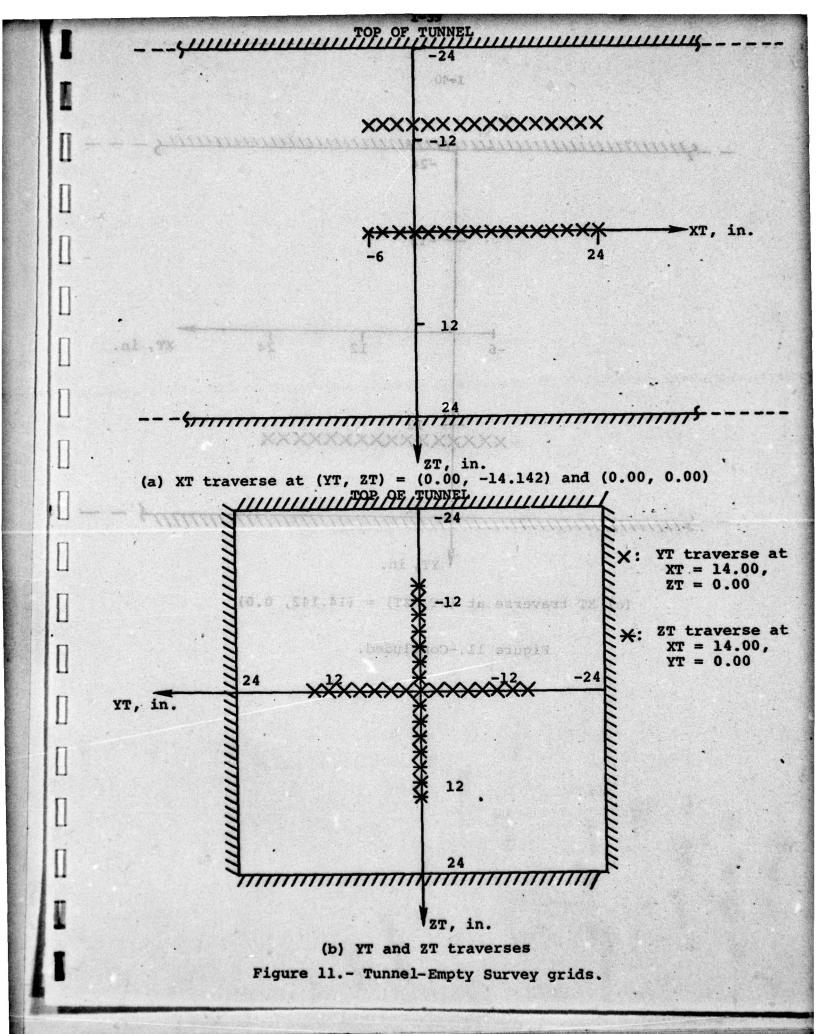
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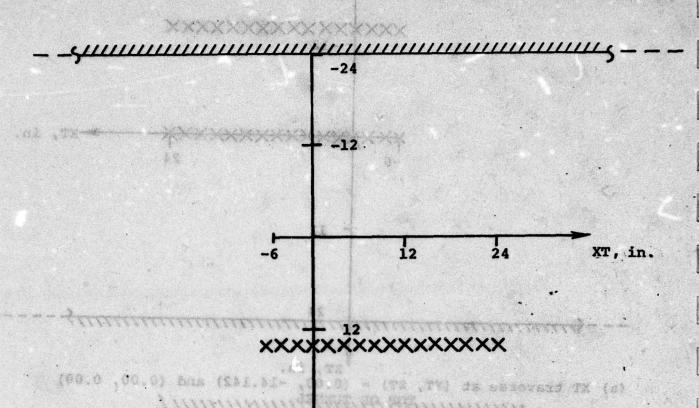
Figure 10.-Measured wing and wing-body quantities.

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(I) Sidewash comparison for (I) (I).

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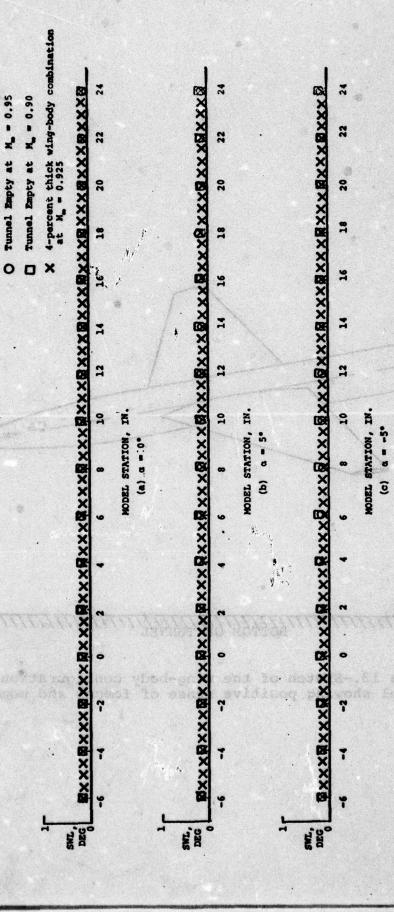


Figure 12.-Local Sidewash SWL at YT = 0.0 in., 2T = -14.14 in.

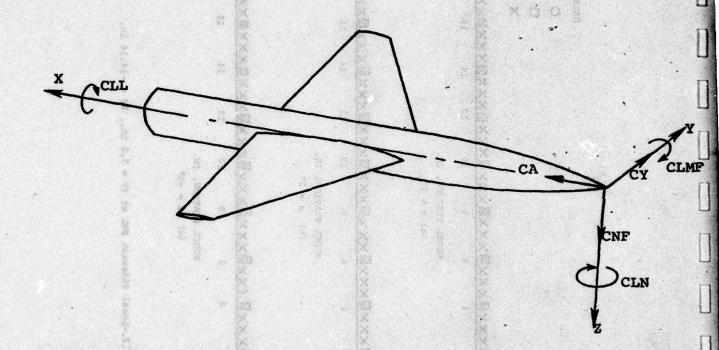


Figure 13.-Sketch of the wing-body configuration in the tunnel showing positive sense of forces and moments.

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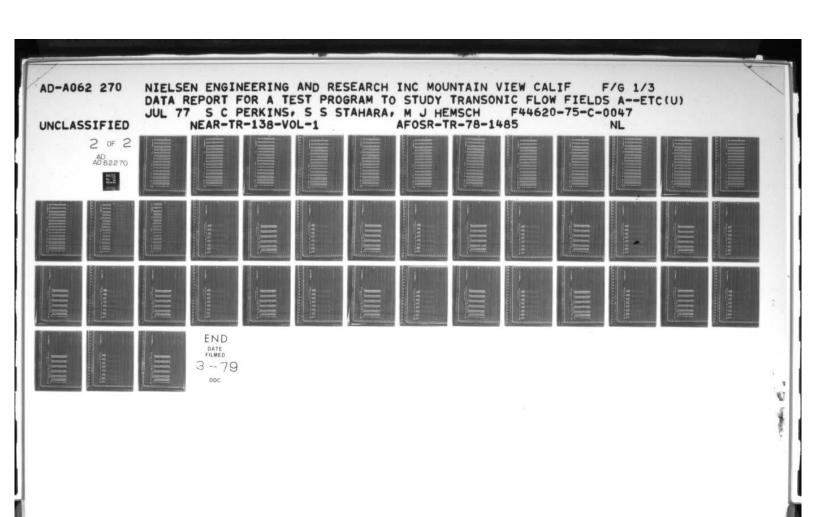
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